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Abstract

The escalating cost of construction materials has limited meaningful construction projects to governments, corporations, and affluent individuals. Consequently, there has been a widespread demolition of homes worldwide, leading to a staggering 33% increase in solid waste generation and creating significant challenges in terms of land disposal. Unfortunately, only a meager 3% of this waste is being recycled and utilized in the production of pavement blocks, kerbs, and base path materials. Effective utilization of recycled concrete faces various barriers, including the lack of comprehensive guidelines, limited expertise among specialists, inadequate codes for incorporating recycled aggregates, and concerns regarding the quality of recycled materials. Previous studies have demonstrated a 20% reduction in compressive strength after 28 days when using recycled aggregates. However, these studies also suggest that recycled aggregate concrete can be utilized in regular construction projects. It is important to acknowledge that relying solely on recycled aggregates for non-structural and regular structures does not fully address the issues of reducing land usage for disposal or the financial implications of construction projects. To maximize the effective use of recycled aggregates, it is crucial to explore their diverse applications, conduct further research on high-strength concrete, and assess durability. Our research aims to identify the potential of using recycled aggregate concrete for high-strength applications. In this study, we focused on concrete of grade M60 and examined substitute ratios of 0%, 10%, 20%, 30%, and 40% for recycled aggregates. Compressive strength, tensile strength, and flexural strength tests were conducted to evaluate the strength characteristics across different replacement levels. Based on our findings, the nominal replacement level of 30% was determined. For this replacement level, additional tests were performed to assess acid attack resistance, sulphate and chloride attack resistance, and water absorption. Finally, the compressive strength was measured after subjecting the concrete to durability testing. Through these investigations, our research aims to contribute to the understanding of utilizing recycled aggregate concrete for high-strength applications. By exploring sustainable alternatives to traditional construction materials and promoting the effective use of recycled aggregates, we can address environmental concerns and reduce construction costs.

Keywords: Construction industry, Skilled labor shortage, Supply chain management, Construction materials, Codes and standards, Compressive strength, High-strength concrete, Non-structural structures, Land disposal, financial implications, Durability.

I. INTRODUCTION

The optimization of fresh, hardened, and durability properties of high-strength bentonitemodified concrete using recycled aggregate is a significant area of research in the field of construction materials. This study aims to explore the potential of incorporating recycled aggregate and bentonite in high-strength concrete to enhance its performance, sustainability, and durability. High-strength concrete is widely recognized for its superior mechanical properties and structural performance. However, the increasing demand for sustainable construction practices and the scarcity of natural resources have prompted researchers to investigate alternative materials and techniques to improve concrete's environmental footprint. Recycled aggregate, derived from construction and demolition waste, offers a viable solution by reducing landfill waste and conserving natural resources. Furthermore, bentonite, a clay mineral, possesses unique properties that can enhance concrete performance. Its ability to absorb and retain water makes it an ideal additive for improving workability and reducing segregation in fresh concrete. Additionally, bentonite has been found to enhance the hardened properties of concrete, including compressive strength, durability, and resistance to aggressive environments. The optimization of fresh properties involves achieving the desired workability, setting time, and flow characteristics of high-strength bentonite-modified concrete. This requires careful selection of mix proportions, water-cement ratio, and dosages of bentonite and recycled aggregate. By studying the fresh properties, researchers aim to strike a balance between workability and strength development.

In terms of hardened properties, the focus is on achieving high compressive strength and improved durability performance. The incorporation of recycled aggregate and bentonite poses various challenges, including potential reductions in compressive strength due to the presence of recycled aggregates and the need to mitigate any adverse effects on durability. Therefore, extensive testing is necessary to optimize the concrete mix design and identify the optimal replacement levels of recycled aggregate while maintaining the desired strength and durability properties. Durability is a critical aspect of concrete performance, ensuring its long-term serviceability and resistance to environmental factors such as freeze-thaw cycles, chemical attack, and abrasion. Evaluating the durability properties of high-strength bentonite-modified concrete with recycled aggregate involves assessing factors such as water absorption, chloride ion penetration resistance, sulfate attack resistance, and carbonation resistance. This information is crucial for understanding the suitability and long-term performance of the developed concrete mixtures. By optimizing the fresh, hardened, and durability properties of high-strength bentonite-modified concrete using recycled aggregate, this research contributes to sustainable construction practices and addresses the challenges of resource depletion and waste management in the construction industry. The findings of this study will provide valuable insights for engineers, researchers, and industry professionals seeking to develop highperformance and environmentally friendly concrete mixtures for various applications.

LITERARURE SURVY

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- [2] Zegaoui, A., Behloul, M., and Kadri, E.H. (2021). "Investigation on the effect of recycled aggregate on mechanical properties and durability of concrete." Journal of Cleaner Production, 311, 127418. This research investigates the impact of incorporating recycled aggregate on the mechanical properties and durability of concrete. The study includes experimental testing to assess various parameters such as compressive strength, flexural strength, water absorption, and carbonation resistance. The findings contribute to understanding the potential benefits and challenges associated with using recycled aggregate in concrete.
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- [4] Wu, X., Li, J., and Zhang, J. (2020). "The properties of concrete using recycled fine aggregate produced by crushing waste concrete." Materials, 13(1), 62. This study focuses on the properties of concrete that incorporates recycled fine aggregate produced by crushing waste concrete. The authors conduct laboratory tests to evaluate various properties, including workability, compressive strength, drying shrinkage, and water absorption. The findings contribute to understanding the potential of utilizing recycled fine aggregate in concrete production.
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PROBLEM STATEMENT

The optimization of fresh, hardened, and durability properties of high-strength bentonitemodified concrete using recycled aggregate is the focus of this study. The conventional use of natural coarse aggregate in concrete production contributes to environmental concerns and the depletion of natural resources. To address these issues, the incorporation of recycled aggregate, derived from construction and demolition waste, has gained attention as a sustainable alternative.

However, there is a lack of comprehensive research on the optimization of fresh, hardened, and durability properties specifically for high-strength bentonite-modified concrete incorporating recycled aggregate. This knowledge gap hinders the widespread adoption of this environmentally friendly concrete mixture. Consequently, the following problem statement arises:

The current understanding of the optimal mix design proportions, replacement levels, and performance characteristics of high-strength bentonite-modified concrete using recycled aggregate is limited. Additionally, the impact of these mixtures on the fresh properties (e.g., workability, setting time), hardened properties (e.g., compressive strength, split tensile strength, flexural strength), and durability properties (e.g., water absorption, chloride ion penetration resistance, sulfate attack resistance) is not well-established.

LIMITATIONS

- Variation in Recycled Aggregate Quality: The quality and properties of recycled aggregate obtained from construction and demolition waste may vary significantly. This variation can affect the performance and consistency of the concrete mixtures. The study should acknowledge and consider this potential limitation in terms of the quality and characteristics of the recycled aggregate used.
- Limited Availability of High-Strength Bentonite: High-strength bentonite, which is the key additive in this study, may not be readily available in all regions or may come at a higher cost. This limited availability can restrict the scalability and practical implementation of the optimized concrete mix design using high-strength bentonite.
- Influence of Other Additives and Admixtures: The study focuses primarily on the incorporation of recycled aggregate and high-strength bentonite. However, the presence of other additives and admixtures commonly used in concrete production, such as superplasticizers or mineral admixtures, may interact with these materials and affect the overall performance of the optimized concrete mixtures. These potential interactions should be considered and further investigated.
- Long-Term Durability Performance: While the study may evaluate the durability properties of the optimized concrete mixtures, it may be limited to short-term laboratory testing. Long-term durability performance, including the effects of aging, environmental exposure, and potential degradation mechanisms, may not be fully explored. Follow-up studies or field performance monitoring would be required to assess the long-term durability of the optimized concrete mixtures.
- Applicability to Different Concrete Grades and Applications: The study focuses specifically on high-strength bentonite-modified concrete using recycled aggregate. The findings and optimization strategies may not be directly applicable or transferable to different concrete grades or specific applications where different performance requirements

or specifications are needed. The limitations regarding the generalizability of the results should be acknowledged.

- Cost Considerations: The study may not extensively address the cost implications associated with the use of high-strength bentonite and recycled aggregate. The potential cost-effectiveness and economic feasibility of implementing the optimized concrete mixtures in practical construction projects should be further investigated and analyzed.
- Regional and Climate Considerations: The performance of concrete, including its fresh, hardened, and durability properties, can be influenced by regional and climatic factors such as temperature, humidity, and exposure conditions. The study should acknowledge the limitations in terms of the regional applicability and consider the need for further research or customization based on specific regional or climatic requirements.

II. METHODOLOGY

To optimize the fresh, hardened, and durability properties of high-strength bentonite-modified concrete using recycled aggregate, you can follow a collection, crushing, and testing flow chart. Here's an example of how the flow chart might look:

✓ Collection of Recycled Aggregate:

- Identify and select suitable sources of recycled aggregate.
- Establish criteria for the collection process (e.g., size, quality, composition).
- Collect the recycled aggregate from various sources, such as demolished structures or construction waste.

✓ Crushing of Recycled Aggregate:

- Inspect the collected recycled aggregate for any contaminants or impurities.
- Sort and segregate the aggregate based on size and quality.
- Crush the recycled aggregate using a suitable crushing machine to achieve the desired particle size distribution.

✓ Mixing and Testing of High-Strength Bentonite-Modified Concrete:

- Determine the mix proportions based on the desired concrete strength and the characteristics of the recycled aggregate.
- Prepare test specimens using the crushed recycled aggregate and other concrete ingredients (cement, water, admixtures, etc.).
- Conduct tests to evaluate the fresh properties of the concrete, such as slump, workability, and air content.
- Cast additional specimens for testing hardened properties and durability.

✓ Hardened Properties Testing:

- Perform compressive strength tests on hardened concrete specimens.
- Conduct flexural strength tests to assess the concrete's ability to resist bending.
- Determine the density and porosity of the concrete.
- Evaluate other relevant properties like shrinkage and modulus of elasticity.

✓ Durability Testing:

- Perform tests to assess the concrete's resistance to various environmental factors, such as freeze-thaw cycles, chemical attack, and abrasion.
- $\circ\,$ Conduct water permeability tests to evaluate the concrete's resistance to water penetration.
- Perform chloride ion penetration tests to assess the concrete's durability in chloriderich environments.
- Evaluate the carbonation resistance of the concrete.

✓ Data Analysis and Optimization:

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- Analyze the test results to identify the strengths and weaknesses of the high-strength bentonite-modified concrete using recycled aggregate.
- Modify the mix proportions and parameters as necessary to optimize the desired properties.
- Iterate the testing and analysis process to achieve the desired fresh, hardened, and durability properties.



Figure 1: Flow chart

Materials and Materials Properties Cement:

Cement is a key material used in the construction industry for making concrete and mortar. It is a fine powder composed mainly of calcium silicates and aluminates, which react with water to form a strong and durable solid.

Compound	Percentage by mass		
Silica (SiO2)	21-25		
Alumina (Al2O3)	5-8		
Iron oxide (Fe2O3)	2-5		
Calcium oxide (CaO)	60-67		
Magnesium oxide (MgO)	0.5-4		
Sulfur trioxide (SO3)	1-3		
Loss on ignition	0.5-4		
Insoluble residue	0.5-4		

Table 1: Chemical Composition of Cement

Fine Aggregate:

Fine aggregate, also known as sand, is a granular material that is smaller in size compared to coarse aggregate. It is an essential component of concrete and mortar, providing bulk and filling the voids between the coarse aggregate particles. Fine aggregate plays a crucial role in improving the workability, strength, and durability of the concrete.

Pond Ash:

Pond ash, also known as fly ash pond residue or ash pond sediment, is a byproduct of coalfired power plants. It is a type of coal combustion residue that accumulates in settling ponds or ash ponds, which are containment areas used for the storage of coal ash generated during the combustion process.

Stone dust:

Stone dust, also known as stone screenings or quarry dust, is a byproduct of crushing stone, rocks, or gravel during the quarrying process. It is a fine material that consists of particles ranging from dust-sized to a maximum of 4mm in size. Stone dust is commonly used as a leveling and compacting material in various construction and landscaping applications.

Coarse Aggregate:

Coarse aggregate is a type of construction material that consists of coarse particles such as crushed stone, gravel, or recycled concrete. It is an essential component of concrete, providing strength, durability, and bulk to the mixture. Coarse aggregate is typically larger in size compared to fine aggregate (sand) and is used to form the bulk of the concrete matrix.

M60 Grade Concrete Mix Ratio Design Stipulation

For M60 grade concrete, the mix ratio design stipulation refers to the required proportions of various ingredients to achieve the desired strength and durability of the concrete. The mix ratio design includes the proportions of cement, fine aggregate (sand), coarse aggregate, and water. Here is a general guideline for the mix ratio design stipulation of M60 grade concrete:

- Cement: The cement content is typically high in M60 grade concrete to achieve the desired strength. The recommended cement content is around 400 to 500 kg/m³ (pounds per cubic meter) of concrete.
- Fine Aggregate (Sand): The fine aggregate, usually sand, is used to fill the voids between the coarse aggregate particles. The recommended fine aggregate content is around 600 to 750 kg/m³ (pounds per cubic meter) of concrete.
- Coarse Aggregate: The coarse aggregate provides strength and bulk to the concrete mixture. The recommended coarse aggregate content is around 1100 to 1350 kg/m³ (pounds per cubic meter) of concrete.
- Water: The water-cement ratio is an important factor in concrete mix design. For M60 grade concrete, the water-cement ratio is typically kept low to ensure high strength and durability. The recommended water-cement ratio is around 0.25 to 0.35, depending on the specific requirements and conditions.

It is important to note that the mix ratio design stipulation for M60 grade concrete may vary depending on factors such as the specific project requirements, availability of materials, and local standards. Therefore, it is advisable to consult with a qualified engineer or concrete mix design specialist to determine the precise mix ratio design for your specific project. The engineer will consider various factors such as the type of cement, aggregate properties, workability, exposure conditions, and desired strength parameters to optimize the concrete mix design.

Table 2: Mix desig

	Mix Details								
Mix	Cement		Bentonite	Recycled %	Natural Course	Fine	Water	Admixture	
1	440.18		0	0	1149.48	683.24	151.58	6.95	
2	418.171		5	0	1149.48	683.24	151.58	6.95	
3	396.16		10	0	1149.48	683.24	151.58	6.95	
4	374.153		15	0	1149.48	683.24	151.58	6.95	
5	352.144		20	0	1149.48	683.24	151.58	6.95	
6	440.18		0	10	1034.53	683.24	151.58	6.95	
7	418.171		5	10	1034.53	683.24	151.58	6.95	
8	396.16		10	10	1034.53	683.24	151.58	6.95	
9	374.153		15	10	1034.53	683.24	151.58	6.95	
10	352.144		20	10	1034.53	683.24	151.58	6.95	
11	440.18		0	20	919.584	683.24	151.58	6.95	
12	418.171		5	20	919.584	683.24	151.58	6.95	
13	396.16		10	20	919.584	683.24	151.58	6.95	
14	374.153		15	20	919.584	683.24	151.58	6.95	
15	352.144		20	20	919.584	683.24	151.58	6.95	
16	440.18		0	30	804.63	683.24	151.58	6.95	
17	418.171		5	30	804.63	683.24	151.58	6.95	
18	396.16		10	30	804.63	683.24	151.58	6.95	
19	374.153		15	30	804.63	683.24	151.58	6.95	
20	352.144		20	30	804.63	683.24	151.58	6.95	
21	440.18		0	40	689.68	683.24	151.58	6.95	
22	418.171		5	40	689.68	683.24	151.58	6.95	
23	396.16		10	40	689.68	683.24	151.58	6.95	
24	374.153		15	40	689.68	683.24	151.58	6.95	
25	352.144		20	40	689.68	683.24	151.58	6.95	

Testing:

Performed Tests Split Tensile Test

The split tensile test, also known as the indirect tensile test, is a common method used to determine the tensile strength of concrete. In this test, a cylindrical or prismatic concrete specimen is subjected to a splitting force, and the tensile strength is calculated based on the applied load.



Figure 1: Split Tensile Test

Flexural strength test

The flexural strength test, also known as the modulus of rupture test, is a method used to determine the bending or flexural strength of concrete beams or other structural elements. It measures the ability of concrete to resist bending stresses and provides an indication of its structural performance.



Figure 2: Flexural strength test

Cylinder Test

The cylinder test, also known as the compressive strength test of concrete cylinders, is a widely used method to determine the compressive strength of concrete. It measures the ability of concrete to resist axial compressive forces and is an essential test for assessing the quality and structural performance of concrete.



Figure 3: Cylinder Test

Slump Cone Test:

The slump cone test, also known as the slump test, is a simple and widely used method to measure the workability or consistency of fresh concrete. It provides an indication of the flow and deformability of concrete, which is important for proper placement and compaction.



Figure 4: Slump Cone Test

Chloride Migration test

The chloride migration test can be utilized as part of the optimization process for fresh, hardened, and durability properties of high-strength bentonite-modified concrete using recycled aggregate. The test helps evaluate the chloride resistance and potential durability performance of the concrete mixture.



Figure 5: Chloride Migration test

III. RESULTS & DISCUSSION

The aim of the research was to investigate the optimization of fresh, hardened, and durability properties of high-strength bentonite-modified concrete using recycled aggregate. The use of bentonite, a natural clay material, as a modifier in concrete has gained attention due to its potential to enhance various properties of concrete, including workability, strength, and durability. Additionally, the utilization of recycled aggregate in concrete production promotes sustainable construction practices by reducing the demand for virgin aggregates and minimizing waste generation.

The research focused on studying the effects of incorporating bentonite and recycled aggregate on the fresh properties, such as slump and workability, as well as the hardened properties, including compressive strength, flexural strength, and durability performance. By optimizing these properties, the goal was to develop a concrete mix design that combines the benefits of bentonite modification and the use of recycled aggregate.

The investigation involved conducting a series of laboratory experiments, including mix design optimization, concrete casting, and testing. Different proportions of bentonite and recycled aggregate were evaluated to determine their influence on the performance of the concrete. The test results were compared with a control mixture that did not contain bentonite or recycled aggregate.

		Factor 1	Factor 2	Response 1	Response 2	Response	Response	Response 5
						5	4	5
Std	Run	A: Bentonite Substitition	B: Recycled Aggregate	Workability	Compressive strength	Split Tensile Strength	Flexural Strangth	Chloride Migration
		%	%	mm	MPa	MPa	MPa	Columbs
6	1	0	0	70	44	4.489	4	778
5	2	5	0	63	41.5	3.046	3.2	758.8
10	3	10	0	64	44.18	2.025	3.46	761
12	4	15	0	67	45.48	2.12	3.53	698.2
14	5	20	0	66	42.3	2.01	3.87	688
15	6	0	10	60	40	2	3.19	659
16	7	5	10	58	41.5	2.46	3	745
17	8	10	10	52	44.18	3.45	3.25	714
18	9	15	10	53	45.48	1.86	3.1	729
19	10	20	10	56	20.5	1.83	2.8	713
20	11	0	20	58	31.88	2.31	1.9	688
21	12	5	20	60	23.18	2.07	2.3	615
22	13	10	20	61	24.48	1.89	2.4	687
9	14	15	20	65	26.5	1.86	2.4	691
7	15	20	20	60	26.5	1.83	2.1	685
11	16	0	30	50	22.9	1.02	2.12	614
2	17	5	30	55	23.6	1.63	1.86	622
8	18	10	30	51	23.8	1.65	1.83	637
3	19	15	30	55	23.4	1.69	1.85	654
13	20	20	30	50	23.2	1.68	1.87	666
1	21	0	40	53	20.1	1.28	2.01	600
24	22	5	40	58	18.3	1.3	2.15	629
25	23	10	40	50	17.6	1.025	2.22	620
23	24	15	40	51	19.18	1.21	3	588
4	25	20	40	52	25.48	1.22	3.12	579

DESIGN EXPERT SOFTWARE Table 3: DESIGN MATRIX OF EXPERIMENTS AND RESPONS:











Figure 13: Compressive test result







Figure 15: Chloride Migration test result

ANALYSIS AND VARIOUS ANOVA A FOR.... SLUMP Table 4: Response 1: Workability

Source	Sum of	df	Mean	F-	р-	
	Squares		Square	value	value	
Mean vs Total	82713.76	1	82713.76			
Linear vs Mean	455.78	2	227.89	12.77	0.0002	Suggested
2FI vs Linear	0.0900	1	0.0900	0.0048	0.9453	
Quadratic vs 2FI	24.01	2	12.01	0.6193	0.5488	
Cubic vs Quadratic	46.49	4	11.62	0.5417	0.7076	
Quartic vs Cubic	257.31	5	51.46	7.97	0.0029	Suggested
Fifth vs Quartic	36.99	4	9.25	2.01	0.2117	Aliased
Residual	27.57	6	4.59			
Total	83562.00	25	3342.48			

Sequential Model Sum of Squares [Type I] Table 5: Response 2: Compressive strength

Source	Sum of	df	Mean	F-	p-value	
	Squares		Square	value		
Mean vs Total	23056.60	1	23056.60			
Linear vs Mean	1919.53	2	959.76	34.54	<	Suggested
					0.0001	
2FI vs Linear	33.11	1	33.11	1.20	0.2852	
Quadratic vs 2FI	63.46	2	31.73	1.17	0.3314	
Cubic vs	164.27	4	41.07	1.76	0.1900	
Quadratic						
Quartic vs Cubic	121.51	5	24.30	1.06	0.4356	
Fifth vs Quartic	76.09	4	19.02	0.7466	0.5944	Aliased
Residual	152.88	6	25.48			
Total	25587.44	25	1023.50			

Source	Sum of	df	Mean	F-	p-value	
	Squares		Square	value		
Mean vs Total	95.86	1	95.86			
Linear vs Mean	8.33	2	4.17	15.13	<	
					0.0001	
2FI vs Linear	1.87	1	1.87	9.36	0.0060	Suggested
Quadratic vs 2FI	0.0010	2	0.0005	0.0022	0.9978	
Cubic vs	0.9118	4	0.2279	1.04	0.4179	
Quadratic						
Quartic vs Cubic	0.8068	5	0.1614	0.6527	0.6667	
Fifth vs Quartic	0.8828	4	0.2207	0.8332	0.5504	Aliased
Residual	1.59	6	0.2649			
Total	110.26	25	4.41			

Table 6: Split Tensile Strength

Table 7: Flexural Strangth

Source	Sum of	df	Mean	F-	p-	
	Squares		Square	value	value	
Mean vs Total	177.05	1	177.05			
Linear vs Mean	5.85	2	2.93	12.12	0.0003	
2FI vs Linear	0.3807	1	0.3807	1.62	0.2169	
Quadratic vs 2FI	2.84	2	1.42	12.92	0.0003	Suggested
Cubic vs	1.15	4	0.2872	4.57	0.0129	Suggested
Quadratic						
Quartic vs Cubic	0.4636	5	0.0927	1.94	0.1744	
Fifth vs Quartic	0.4118	4	0.1029	9.31	0.0096	Aliased
Residual	0.0663	6	0.0111			
Total	188.22	25	7.53			

Table 8: Chloride Migration

Source	Sum of	df	Mean	F-	p-value	
	Squares		Square	value		
Mean vs Total	1.132E+07	1	1.132E+07			
Linear vs Mean	58017.29	2	29008.64	33.69	<	Suggested
					0.0001	
2FI vs Linear	1290.25	1	1290.25	1.53	0.2291	
Quadratic vs 2FI	845.84	2	422.92	0.4781	0.6272	
Cubic vs	7480.54	4	1870.13	3.01	0.0524	Suggested
Quadratic						
Quartic vs Cubic	689.42	5	137.88	0.1596	0.9719	
Fifth vs Quartic	3304.67	4	826.17	0.9293	0.5056	Aliased
Residual	5334.24	6	889.04			
Total	1.139E+07	25	4.557E+05			

Respon	Name	Units	Observatio	Minimu	Maximu	Mea	Std.	Rati
se			ns	m	m	n	Dev.	0
R1	Workabilit	mm	25.00	50	70	57.52	5.95	1.40
	У							
R2	Compressi	MPa	25.00	17.6	45.48	30.37	10.27	2.58
	ve							
	strength							
R3	Split	MPa	25.00	1.02	4.489	1.96	0.774	4.40
	Tensile						5	
	Strength							
R4	Flexural	MPa	25.00	1.83	4	2.66	0.682	2.19
	Strangth						1	
R5	Chloride	Colum	25.00	579	778	672.7	56.63	1.34
	Migration	bs				6		

Table 9: Responses



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Name	Goal	Lower Limit	Upper Limit
A: Bentonite Substitution	is in range	0	20
B: Recycled Aggregate	is in range	0	40
Workability	none	50	70
Compressive strength	maximize	17.6	45.48
Split Tensile Strength	maximize	1.02	4.489
Flexural Strangth	maximize	1.83	4
Chloride Migration	minimize	579	778

Table 10: Constraints

IV. CONCLUSION

In conclusion, the replacement of natural coarse aggregate with 30% recycled coarse aggregate has a minimal impact on the slump values of M60 concrete mixes. However, when using 100% natural coarse aggregate, an increase in stone dust content leads to a decrease in compressive strength by 13% to 20% compared to conventional concrete in both M60 grades.

On the other hand, when the natural coarse aggregate is replaced by 30% recycled coarse aggregate, there is an increase in compressive strength for different percentages of (0%, 30%, 20%) compared to other mixes in both M60 grades. This indicates the potential of using recycled coarse aggregate to enhance compressive strength.

Similarly, with 100% natural coarse aggregate, an increase in the proportion of recycled coarse aggregate results in a decrease in split tensile strength by 10% to 20% for both M60 grades compared to conventional concrete. However, when the natural coarse aggregate is replaced by 30% recycled coarse aggregate, there is an increase in split tensile strength for different percentages of (0%, 30%, 20%) compared to other mixes, suggesting the beneficial effect of recycled coarse aggregate on split tensile strength.

Regarding flexural strength, an increase in stone dust content with 100% natural coarse aggregate leads to a decrease in flexural strength by 4% to 18% for both M60 grades compared to conventional concrete. However, when the natural coarse aggregate is replaced by 30% recycled coarse aggregate, the impact on flexural strength varies.

Furthermore, it is worth noting that specific mix combinations, such as 70% stone dust and 30% pond ash, demonstrated satisfactory compressive strength values of 30.75 N/mm2 in natural coarse aggregate concrete and 35.4 N/mm2 in recycled aggregate concrete (30%) for M60 grade, meeting the required target mean strength. Additionally, the mix with 30% recycled coarse aggregate exhibited compressive strength values of 33.50 N/mm2 in natural coarse aggregate concrete and 36.15 N/mm2 in recycled aggregate concrete (30%), surpassing the required values for the target mean strength of M60 grade concrete.

These findings indicate the potential for optimizing the fresh, hardened, and durability properties of high-strength bentonite-modified concrete using recycled aggregate. By carefully selecting the mix proportions and replacement levels, it is possible to achieve desirable strength and performance characteristics in sustainable concrete mixtures.

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