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SIGNIFICANCE OF SHAPE FACTOR AND DIFFERENT HEAT SOURCES AND ON A WATER BASED HYBRID NANOFLUID FLOW OVER A SHRINKING SHEET WITH VARIABLE VISCOSITY

Potiapula Usnarani ² , B. Kavindra Keddy ²	pula Usharani ^{1*} , B. Ravindra R	keddy ²
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Abstract

Objective of this study is to examine the influence of the variable viscosity, thermal radiation and exponential heat source parameters on a hybrid nanofluid (Water + Multi-Walled Carbon Nanotubes (*MWCNT*) + Copper (II) oxide (*CuO*)) flow over a shrinking sheet with suction. Governing equations, which are partial differential equations, are converted into the system of nonlinear ordinary differential equations by using appropriate similarity transformations and this system has been solved using the bvp4c solver. The heat transmission rate and friction factor against the pertinent parameters are explained using bar graphs. It is observed that, at $0 \le \phi_{MWCNT} \le 0.09$, (the volume fraction of *MWCNT*) the skin friction coefficient increases at a rate of 7.828962 (in case of Platelet)) and 7.826693 (in case of Cylinder). It is noticed that the rise in magnetic field parameter (*Mg*) and exponential heat source (*Q_e*) decrease the Nusselt number. It is noticed that, when $0.1 \le Q_e \le 0.7$, the heat transfer rate (Nusselt number) is found to decrease by 0.43786 (in case of Platelet) and 0.43137 (in case of Cylinder). It has been found that when the magnetic field parameter upsurges, the velocity declines. Furthermore, it is detected that the increase in thermal radiation enhances the fluid temperature.

Keywords: Thermal radiation, Hybrid nanofluid, Shrinking sheet, Exponential heat source, Suction.

¹Research Scholar, Department of Mathematics, JNTUH-Hyderabad, Kukatpally – 500085, India. Usharani471981@gmail.com

 2 Professor, Department of Mathematics, JNTUH-Hyderabad, Kukatpally – 500085, India. rbollareddy@gmail.com

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σ Electrical conductivity	η Similarity variable		
Pr Prandtl number	σ^* Stefan-Boltzmann constant		
<i>k</i> * Mean absorption coefficient	Mg Magnetic field Parameter		
v Kinematic viscosity	u, v Components of velocity in two (x, y		
<i>k</i> Thermal conductivity)		
ϕ_{MWCNT} Volume fraction of multi-walled	directions		
carbon nanotube	<i>Ra</i> Thermal radiation parameter		
ϕ_{CuO} Volume fraction of Copper (II) Oxide	q_e Coefficient of Exponential Space		
g Acceleration due to gravity	related heat Source		
λ Mixed convection parameter	q_t Coefficient of Thermal dependent		
C_p Specific heat capacity	heat Source		
v_w Mass flux velocity			
δ Temperature dependent fluid viscosity	S Mass transfer parameter		
parameter	where $S > 0$ indicates suction and		
β_T Thermal expansion coefficient	S < 0 indicates injection		
	κ, a Constants and $a > 0$ for liquids		

Nomenclature

1 Introduction

Recent years have seen a number of studies that examine the effects of changing the thermo-physical characteristics of the working fluid on the transmission of heat. Due to its improved thermal conductivity and convective coefficient of heat transmission in contrast to the base fluid, nanofluid has been employed in numerous real engineering sectors, including the energy supply, photonics, and electronics industries (M'hamed et al. [1]). Singh et al. [2] studied the thermal conductivity and viscosity properties of a commercial SiCwater nanofluid. Thermal conductivity is observed to rise with particle loadings and to be greater than the expectations of effective medium theory (EMT) for noninteracting spheres. The steady boundary layer flow of a nanofluid through a moving semi-infinite flat plate was theoretically investigated by Bachok et al. [3]. Dual solutions are seen to exist when

the plate and the free stream flow are moving in different directions. Das et al. [4] used the Runge-Kutta-Fehlberg technique to investigate the magnetic field and solar radiation's effects on the nanofluid's slippery flow on a stretching surface. The thickness of the thermal boundary layer is found to grow proportionally with the slip velocity. The flow of a magnetic nanofluid over a stretched plate subjected to thermal radiation was studied quantitatively by Sheikholeslami et al. [5]. The results show that an increase in magnetic parameter causes a thinning of the hydraulic boundary layer. The boundary layer flow of a nanofluid over a variable viscosity wedge was studied by Das et al. [6]. The skin friction coefficient is found to increase as the Brownian motion parameter rises. Rasool et al. [7] discussed a MHD Darcy-Forchheimer nanofluid flow over a nonlinear stretching sheet with Brownian motion and thermophoresis parameters.

Using a Riga plate emitting nonlinear thermal radiation, Abdul Hakeem et al. [8] examined various nanofluid flows. As can be seen, the temperature ratio parameter helps to improve the temperature distribution. Basha and Sivaraj [9] numerically the transport analysed characteristics of blood based nanofluid flow over the plate and wedge towards a stagnation point. Later, different scholars [10-12] described various nanofluid flows via distinct geometries. When compared to mono fluids, the heat transmission properties of hybrid fluids are superior. These are finding uses in an extensive diversity of fields, from solar energy to air conditioning. Under a constant heat flux boundary condition, Suresh et al. [13] studied the laminar heat transfer and frictional properties of a water-based hybrid nanofluid with a 0.1% volume concentration as it passed through a straight circular tube. Compared to pure water, the experimental findings of using a hybrid nanofluid for laminar flow indicated a maximum improvement in Nusselt number of 13.56 percent at a Reynolds number of 1730. Labib et al. [14] discussed the hydrodynamic and thermal behaviour of laminar forced convection flow nanofluids inside the uniformly heated tube. Threedimensional rotating flow of water-based hybrid nanofluid across a stretched surface with thermal radiation, heat generation, and chemical reaction was investigated by Hayat and Nadeem [15]. In the presence of a Cattaneo-Christov heat flux model. Jamshed and Aziz [16] conducted a computational analysis of heat transfer and entropy generation for boundary layer flow hybrid Casson of conventional and nanofluids. The fluid flow and heat transmission characteristics of a waterbased hybrid nanofluid flow through a stretching cylinder subjected to Joule

heating and viscous dissipation were studied by Maskeen et al. [17]. It has been shown that the presence of hybrid material increases the convective heat transfer, which is at its lowest in the case of copper/water nanofluid. Several studies [18 - 22] then discussed various hybrid nanofluid flows over different geometries.

In view of the preceding research, nobody has up until now tried to explain the significance of variable viscosity and shape factor effects, for the radiative hybrid nanofluid (Water + MWCNT + CuO) flow with exponential heat source. Engineering parameters of concern including friction factor are explained using bar graphs.

2 Mathematical Formulation

A laminar and steady radiative hybrid nanofluid flow (Water + MWCNT + CuO) flow with variable viscosity and exponential heat source is considered in this study and flat plate is assumed as a geometry. Thermophysical characteristics of water (base fluid), MWCNT and CuO(nanoparticles) are shown in Table 1. Following are the assumptions for the current study:

(i) x-axis is taken as along the plate (parallel to the flow), while the y-axis will be transverse to it, as shown in Fig. 1.

(ii) There is a magnetic field employed in the direction of y-axis, with a strength of B_0 .

(iii) The shrinking velocity of the sheet is $u_w = -ax$ with a > 0 being shrinking constant.

(iv) Joule heating, induced magnetic field and viscous dissipation are neglected.



Fig. 1 Schematic diagram

These assumptions lead to the following governing equations and boundary conditions (Al-Kouz et al. [23]):

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = \frac{1}{\rho_{hnf}}\frac{\partial}{\partial y}\left(\mu_{hnf}\frac{\partial u}{\partial y}\right) + g\beta_T \left(T - T_{\infty}\right) - \frac{\sigma_{hnf}}{\rho_{hnf}}B_0^2 u$$
(2)

$$\left(\rho C_{p}\right)_{hnf}\left(u\frac{\partial T}{\partial x}+v\frac{\partial T}{\partial y}\right)=k_{hnf}\frac{\partial^{2}T}{\partial y^{2}}+\frac{16\sigma^{*}T_{\infty}^{3}}{3k^{*}}\frac{\partial^{2}T}{\partial y^{2}}+q_{e}\left(T_{w}-T_{\infty}\right)\exp\left(-my\sqrt{\frac{a}{v}}\right)$$

$$+a\left(T_{w}-T_{w}\right)$$
(3)

$$\begin{aligned} &+q_t \left(T - T_{\infty} \right) \\ &\text{at } y = 0 : u = u_w, v = v_w, T = T_w, \\ &\text{as } y \to \infty : u \to 0, T \to T_{\infty}. \end{aligned}$$

$$(4)$$

)

2.1 Hybrid nanofluid (HNF) thermophysical characteristics

$$\begin{split} \left(\rho C_{p}\right)_{hnf} = & \left[\left(1-\phi_{MWCNT}\right)\left(\rho C_{p}\right)_{f} + \phi_{MWCNT}\left(\rho C_{p}\right)_{MWCNT}\right]\left(1-\phi_{CuO}\right) + \left(\rho C_{p}\right)_{CuO}\phi_{CuO}, \\ \sigma_{nf} &= \frac{\sigma_{MWCNT} + 2\sigma_{f} - 2\sigma_{f}\phi_{MWCNT} + 2\sigma_{MWCNT}\phi_{MWCNT}}{\sigma_{MWCNT} + 2\sigma_{f} + \sigma_{f}\phi_{MWCNT} - \sigma_{MWCNT}\phi_{MWCNT}} \times \sigma_{f}, \\ \rho_{hnf} &= & \left[\left(1-\phi_{MWCNT}\right)\rho_{f} + \phi_{MWCNT}\rho_{MWCNT}\right]\left(1-\phi_{CuO}\right) + \rho_{CuO}\phi_{CuO}, \\ \mu_{hnf} &= \frac{\mu_{f}}{\left(1-\phi_{MWCNT}\right)^{2.5}\left(1-\phi_{CuO}\right)^{2.5}}, \\ \sigma_{hnf} &= \frac{\sigma_{CuO} + 2\sigma_{nf} - 2\sigma_{nf}\phi_{CuO} + 2\sigma_{CuO}\phi_{CuO}}{\sigma_{CuO} + 2\sigma_{nf} + \sigma_{nf}\phi_{CuO} - \sigma_{CuO}\phi_{CuO}} \times \sigma_{nf}. \end{split}$$

and

$$k_{hnf} = \frac{k_{CuO} + (n+1)k_{nf} - (n+1)k_{nf}\phi_{CuO} + (n+1)k_{CuO}\phi_{CuO}}{k_{CuO} + (n+1)k_{nf} + k_{nf}\phi_{CuO} - k_{CuO}\phi_{CuO}} \times k_{nf},$$

$$k_{nf} = \frac{k_{MWCNT} + (n+1)k_{f} - (n+1)k_{f}\phi_{MWCNT} + (n+1)k_{MWCNT}\phi_{MWCNT}}{k_{MWCNT} + (n+1)k_{f} + k_{f}\phi_{MWCNT} - k_{MWCNT}\phi_{MWCNT}} \times k_{f}.$$

(Sheikholeslami and Rokni [24])

The shape parameter is denoted by n here. Several shapes of nanoparticles are represented in Table 1 with their corresponding shape factors.

Note that the variable viscosity coefficient μ_f is defined as (Nadeem et al. [25]):

$$\frac{1}{\mu_f} = \frac{1}{\mu_{f\infty}} \Big[1 + \kappa \big(T - T_v \big) \Big] \text{ or } \frac{1}{\mu_f} = a \big(T - T_v \big)$$

where $a = \frac{\kappa}{\mu_{f\infty}}$ and $T_v = T_\infty - \frac{1}{\kappa}$.

Table 1 Nanoparticle forms and values of their respective shape factors (Sheikholeslami and Rokni [24])

S. No.	Name of the shape	п
1	Platelet	5.7
2	Cylinder	4.8

S. No.		H_2O	MWCNT	CuO
		(f)	$(\phi_{\scriptscriptstyle MWCNT})$	$\left(\phi_{\scriptscriptstyle CuO} ight)$
1	$ ho(kgm^{-3})$	997.1	2100	6320
2	$k\left(W\left(m\ K ight)^{-1} ight)$	0.613	3000	76.5
3	$C_p\left(J\left(kg\ K\right)^{-1}\right)$	4179	711	531.8
4	$\sigma(Sm^{-1})$	0.0000055	0.00019	2.7x10 ⁻⁸

Table 2 Thermophysical property values for base fluid and nanomaterials (Alzahrani et al.[26])

Das et al. [27] recommended the succeeding similarity variables to alter controlling equations:

$$u = axf'(\eta), v = -\sqrt{av}f, \eta = y\sqrt{\frac{u_w}{vx}}, \theta(\eta) = \frac{T - T_{\infty}}{T_w - T_{\infty}}.$$

(5)

Then (5) makes (1) to fulfil and redraft (2 -4) as:

$$\frac{1}{A_{1}A_{2}}\frac{\delta}{\delta-\theta}f'''+ff''-f'^{2}+\frac{1}{A_{1}A_{2}}\frac{\delta}{\left(\delta-\theta\right)^{2}}f''\theta'+\lambda\theta-\frac{A_{3}Mg}{A_{1}}f'=0$$
(6)

$$\frac{A_{4}}{A_{5}}\frac{1}{\Pr}\theta''+\frac{1}{A_{5}}\frac{Ra}{\Pr}\theta''+f\theta'+\frac{Q_{e}}{A_{5}}\exp\left(-m\eta\right)+\frac{Q_{t}}{A_{5}}\theta=0$$
(7)
at $\eta=0: f(\eta)=S, f'(\eta)=-1, \theta(\eta)=1$
at $\eta\to\infty: f'(\eta)\to 0, \theta(\eta)\to 0$
(8)

where

$$\delta = -\frac{1}{\kappa (T_w - T_w)}, Mg = \frac{\sigma B_0^2}{\rho a}, \Pr = \frac{\mu C_p}{k}, Ra = \frac{16\sigma * T_w^3}{3kk *},$$
$$\lambda = \frac{Gr}{\operatorname{Re}_x^2}, Gr = \frac{g\beta_T (T_w - T_w)x^3}{\upsilon^2}, \operatorname{Re}_x = \frac{xu_w}{\upsilon}, Q_e = \frac{q_e}{a(\rho C_p)},$$
$$Q_t = \frac{q_t}{a(\rho C_p)}, S = -\frac{v_w}{\sqrt{a\upsilon}}.$$

and

$$\begin{aligned} A_{2} &= \left(1 - \phi_{MWCNT}\right)^{2.5} \left(1 - \phi_{CuO}\right)^{2.5}, \\ A_{5} &= \left(1 - \phi_{CuO}\right) \left[\left(1 - \phi_{MWCNT}\right) + \phi_{MWCNT} \frac{\left(\rho C_{p}\right)_{MWCNT}}{\left(\rho C_{p}\right)_{f}} \right] + \phi_{2} \frac{\left(\rho C_{p}\right)_{CuO}}{\left(\rho C_{p}\right)_{f}}, \\ A_{31} &= \frac{\sigma_{MWCNT} + 2\sigma_{f} - 2\phi_{MWCNT} \left(\sigma_{f} - \sigma_{MWCNT}\right)}{\sigma_{MWCNT} + 2\sigma_{f} + \phi_{MWCNT} \left(\sigma_{f} - \sigma_{MWCNT}\right)}, \\ A_{1} &= \left(1 - \phi_{CuO}\right) \left[\left(1 - \phi_{MWCNT}\right) + \phi_{MWCNT} \frac{\rho_{MWCNT}}{\rho_{f}} \right] + \phi_{CuO} \frac{\rho_{CuO}}{\rho_{f}}, \\ A_{3} &= \frac{\sigma_{CuO} + 2A_{31}\sigma_{f} - 2\phi_{CuO} \left(A_{31}\sigma_{f} - \sigma_{CuO}\right)}{\sigma_{CuO} + 2A_{31}\sigma_{f} + \phi_{CuO} \left(A_{31}\sigma_{f} - \sigma_{CuO}\right)} A_{31}, A_{4} &= \frac{k_{CuO} + 2A_{41}k_{f} - 2\phi_{CuO} \left(A_{41}k_{f} - k_{CuO}\right)}{k_{CuO} + 2A_{41}k_{f} + \phi_{CuO} \left(A_{41}k_{f} - k_{CuO}\right)} A_{41}, \\ A_{41} &= \frac{k_{MWCNT} + 2k_{f} - 2\phi_{MWCNT} \left(k_{f} - k_{MWCNT}\right)}{k_{MWCNT} + 2k_{f} + \phi_{MWCNT} \left(k_{f} - k_{MWCNT}\right)}. \end{aligned}$$

Coefficient of skin friction coefficient (C_{fx}) is outlined as:

$$Cf = \frac{\tau_w}{\rho_f u_w^2} \bigg|_{y=0},$$
(9)

where $\tau_w = \mu_{hnf} \left(\frac{\partial u}{\partial y} \right)$.

Rewriting the expression in (9) with (5) yields

$$\sqrt{\operatorname{Re}_{x}}Cf = \frac{1}{A_{2}}f''(0).$$

The following formula can be used to calculate the Nusselt number:

$$Nu_{x} = -\frac{xq_{w}}{k_{f}\left(T_{w} - T_{\infty}\right)}\Big|_{y=0},$$
(10)
where $q_{x} = \left(k_{w} + \frac{16\sigma * T_{\infty}^{3}}{16\sigma * T_{\infty}^{3}}\right)\frac{\partial T}{\partial T}.$

where
$$q_w = \left(k_{hnf} + \frac{16\sigma * T_{\infty}^3}{3k*}\right) \frac{\partial T}{\partial y}.$$

The formula in (10) is reworked with the help of (5) as:

$$\sqrt{\frac{1}{\operatorname{Re}_{x}}}Nu_{x} = -A_{4}(1+Ra)\theta'(0).$$

3 Discussion of outcomes

In order to solve equations (6 - 7) with the conditions (8), the built-in function bvp4c of MATLAB is employed.

3.1 Profiles of Engineering Parameters of Concern

According to Figs. 2 - 3, it has been noted that the rise in Mg and ϕ_{MWCNT} enhance the skin friction coefficient. It is observed that, at $0 \le \phi_{MWCNT} \le 0.09$, the skin friction coefficient

increases at a rate of 7.828962 (in case of Platelet)) and 7.826693 (in case of Cylinder). It is noticed from Figs. 4 – 5 that the rise in Mg and Q_e decrease the Nusselt number. It is noticed that, when $0.1 \le Q_e \le 0.7$, the heat transfer rate (Nusselt number) is found to decrease by 0.43786 (in case of Platelet) and 0.43137 (in case of Cylinder).



Fig. 2 Profile of skin friction coefficient with the impact of Mg



Fig. 3 Profile of skin friction coefficient profile with the impact of ϕ_{MWCNT}



Fig. 4 Profile of Nusselt number with the impact of Mg



Fig. 5 Profile of Nusselt number with the impact of Q_e

3.2 Temperature and Velocity Profiles

As a result of the thermal radiation parameter, heat is transferred to the fluid. There will be a greater transfer of heat energy from the source to the fluid if this value is made larger. Therefore, as seen in Fig. 6, the temperature rises as the fluid particles absorb heat energy. From Fig. 7, it is clear that the rise in Q_e enhances the fluid temperature. It is because of the extra heat supplied to the liquid system by the ESHS (Heat Source related to Exponential space) mechanism. Fig. 8 exhibits the fact that the fluid temperature enriches with the upsurge in Q_t . In Fig. 9, we can see that when ϕ_{MWCNT} increases, the fluid's temperature increases. It has been found, as shown in Fig. 10, that when the magnetic field parameter upsurges, the velocity declines. Magnetic flow lines travelled normally through the fluid when an external magnetic field was applied around it. Particles' movement from one layer to another is impeded as a result of the Lorentz force that is created. Due to this, the fluid's molecules travel very slowly. The fluid's velocity slows as a result. According to the Fig. 11, it has been established that an increase in δ results in a decrease in velocity.



Fig. 6 Profile of $\theta(\eta)$ with the impact of *Ra*



Fig. 7 Profile of $\theta(\eta)$ with the impact of Q_e



Fig. 8 Profile of $\theta(\eta)$ with the impact of Q_t



Fig. 9 Profile of $\theta(\eta)$ with the impact of $\phi_{_{MWCNT}}$



Fig. 10 Profile of $f'(\eta)$ with the impact of Mg



Fig. 11 Profile of $f'(\eta)$ with the impact of δ

4 Conclusions

Objective of this paper is how thermal radiation and variable viscosity parameters effect the characteristics of hybrid nanofluid (Water + MWCNT + CuO) flow over a shrinking sheet with different heat source parameters. The study's findings are briefly summarised below.

- It is observed that, at $0 \le \phi_{MWCNT} \le 0.09$, (the volume fraction of *MWCNT*) the skin friction coefficient increases at a rate of 7.828962 (in case of Platelet)) and 7.826693 (in case of Cylinder).
- It is noticed that the rise in magnetic field parameter (Mg) and exponential heat source (Q_e) decrease the Nusselt number.
- It is noticed that, when $0.1 \le Q_e \le 0.7$, the heat transfer rate (Nusselt number) is found to

decrease by 0.43786 (in case of Platelet) and 0.43137 (in case of Cylinder).

- It has been found that when the magnetic field parameter upsurges, the velocity declines.
- It is detected that the increase in thermal radiation enhances the fluid temperature.

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